



IJEAST

INTERNATIONAL JOURNAL
OF ENGINEERING APPLIED SCIENCE
AND TECHNOLOGY



VOLUME : 9 ISSUE : 10 Print / Issue Publication Date: 21-Apr-2025



ISSN : 2455-2143



DOI : 10.33564/IJEAST.2025.v09i10.005

Indexed In



WWW.IJEAST.COM

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ANALYSIS OF EEMD BASED RESIDUAL SIGNAL FOR BEARING FAULT DIAGNOSIS.

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Abstract—The present study investigated the use of ensemble empirical mode decomposition (EEMD) based residual signals for the condition monitoring and fault diagnosis in the bearings. The acquired signals were decomposed using EEMD technique to obtain intrinsic mode functions (IMFs). For further processing the sensitive IMFs were selected on the basis of their similarity index with the original signal. The residual signal is then obtained by subtracting the ineffective IMFs from the effective IMFs. After that the five statistical features (namely: Root mean square value (RMS), crest factor (CF), peak-to-RMS (pk2rms), impulse factor (IF) and kurtosis (Ku)) and five entropy based features (namely: Approximate entropy (ApEn), permutation energy (PE), Sample entropy (SampEn), dispersion entropy (DE), and fuzzy entropy (FzEn)) were extracted from residual signal. The extracted features were fed to the two state-of-the-art classifiers, support vector machine (SVM) and random forest (RF) for the classification of different bearing faults. The analysis of results shows that the proposed method has potential for identifying and classifying different bearing's faults

Keywords—Vibration analysis, Fault diagnosis, EEMD, Residual signals.

I. INTRODUCTION

A bearing is a rotating machine element which supports the load, provides relative motion with minimum friction. Rolling contact bearings are also called anti friction bearings and these types of bearings are not suitable for shock loads due to poor damping and balls are subjected to plastic deformation under

shock loads leading to noise and vibrations (Tandon and Choudhury, 1999).The health of the machine can be determined by condition monitoring techniques (CMTs).(Jardine et al., 2006).The vibration signal is highly sensitive to bearing status, allowing characteristic information closely related to bearing failure to be extracted. Fourier transform, wavelet transform, and Empirical Mode Decomposition (EMD) are extensively used methods for extracting vibration signal features. EMD has higher signal processing capabilities than the two approaches discussed above, allowing it to effectively analyze signals with more complicated features. It has been observed that EEMD is very promising to denoise the complex machine signals. It is combined with different entropy approach for the machine fault diagnosis. The entropy has been proved as a good indicator to reflect system complexity. But most of the entropy methods are sensitive to selected parameters. In the present study the EEMD is used as denoising techniques and five statistical and five entropy parameters are considered as feature vectors to reflect the condition of the bearing. The efficacy of the proposed methodology is checked by the two state-of-art classifiers: support vector machine (SVM) and random forest.

II. PROPOSED METHODOLOGY

The flowchart describing the experimental methodology is detailed in Fig. 4. First of all, data acquisition of vibration signals from both healthy and damaged bearing was done. Then decomposing and denoising of each the segmented sub-signal was performed using EEMD. Significant IMFs are selected on the basis of their similarity index with original signal based upon the dynamic time wrapping (DTW)

algorithm. Residual signal is obtained by subtracting the sum of ineffective IMFs from the sum of significant IMFs. Statistical features of each of the selected IMF the statistical features are computed. Finally calculated features are used to describe the states of the bearing via classification through RF.

Statistical features that better describes the health conditions of the roller bearings were extracted. Adopting the supervised machine learning through classifiers based on SVM and RF raises diagnosis accuracy.

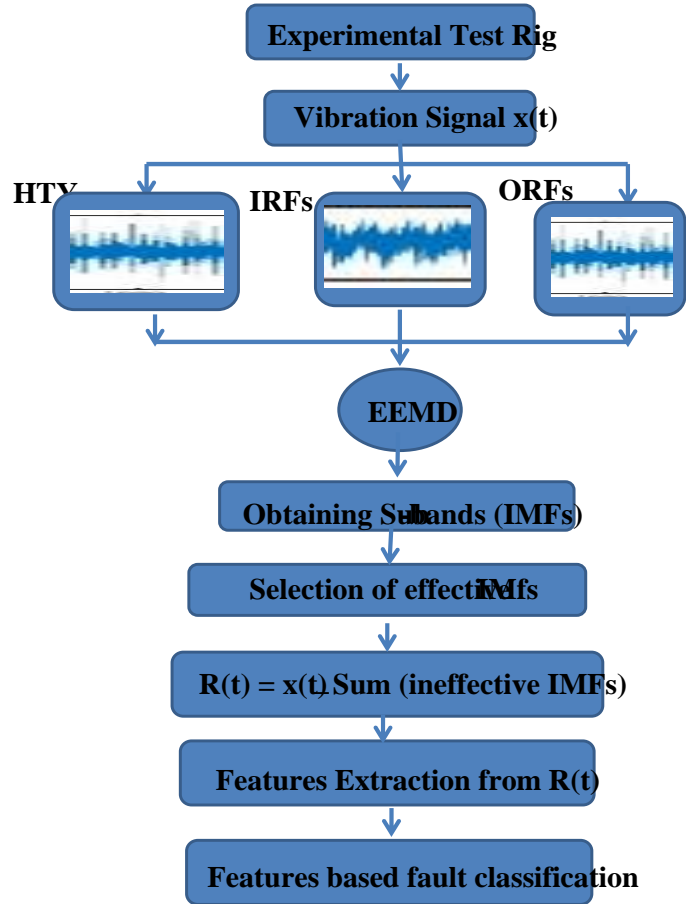


Fig. 1 Experimental methodology

III. EXPERIMENTAL TEST RIG

The experimental rig, as shown in Fig.2, is basically an electro-mechanical system. The motor-side bearing is the component under examination.



Fig.2 Bearing test rig

Electro-discharge Machining was used to seed localized defects on inner and outer races, with varying degrees of damage. The point defects with the diameter ranging from 3 to 5 mm were introduced. The bearing was operated at six distinct speeds, ranging from 25 to 50 Hz. The speed's variation, is attained by variable frequency drive (VFD). Data was collected at a sampling rate of 65500 k samples/s. The acquired experimental data is detailed in Table1, where, (i). HTY is data for healthy bearing (ii). IRF is bearing data with inner race fault (iii). ORF is bearing data with outer race fault

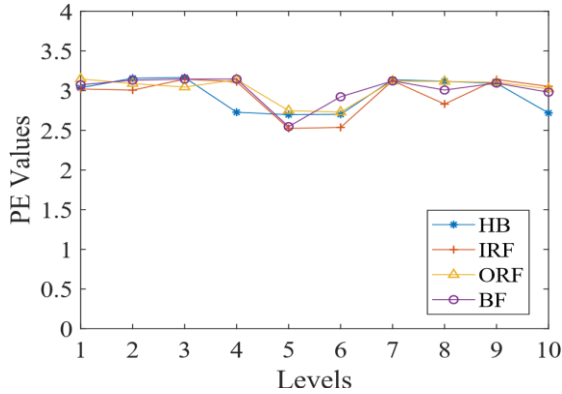


Fig.3 PE values at different levels



Fig.4 Tests bearings with IRF

There are a total of 40 experimental signals that are tabulated in Table1. The 6 signals denote a healthy bearing state, while the 36 signals are acquired for faulty bearing. With a sampling time of 5.2 seconds, 65,536 data points were taken for each recorded signal.

Table -1 Experimental conditions (* -available data)
Speed (Hz)

| Bearing condition | Fault severity (in mm) | Speed (Hz) | | | | | |
|-------------------|------------------------|------------|-------|-------|-------|-------|-------|
| | | 25 Hz | 30 Hz | 35 Hz | 40 Hz | 45 Hz | 50 Hz |
| <i>HTY</i> | - | * | * | * | * | * | * |
| <i>IRF</i> | 3 | * | * | * | * | * | * |
| | 4 | * | * | * | * | * | * |
| | 5 | * | * | * | * | * | * |
| <i>ORF</i> | 3 | * | * | * | * | * | * |
| | 4 | * | * | * | * | * | * |
| | 5 | * | * | * | * | * | * |

IV. EXPERIMENTAL ANALYSIS

In this research work the dynamic response of the system with healthy bearing for different speeds their time-domain representation are obtained and plotted in Figure 5. The time domain graphs for the healthy bearing, with an operating speed of 25-50 Hz, are shown in Fig. 5(a)-(f). With increase in the fault severity the overall vibration amplitude is increased and this increase can be observed from Fig. 6. The figure is plotted for the IR_{Fa} with the fault severity of 3 mm at different

operating speeds. Figure 6 (a) is plotted for operating speed of 25 Hz and then plots for the various speeds are obtained in Fig. 6 (b)-(f), respectively. Similar trends can be observed in Figure 7 for the bearings with OR_{Fa} with the fault severity of 3m. Fig. 7(a)-(d) are the time domain representation of signals acquired for the bearing with faulty outer race at variable speed conditions. The impulses in the signal are indicative of the faulty bearing.

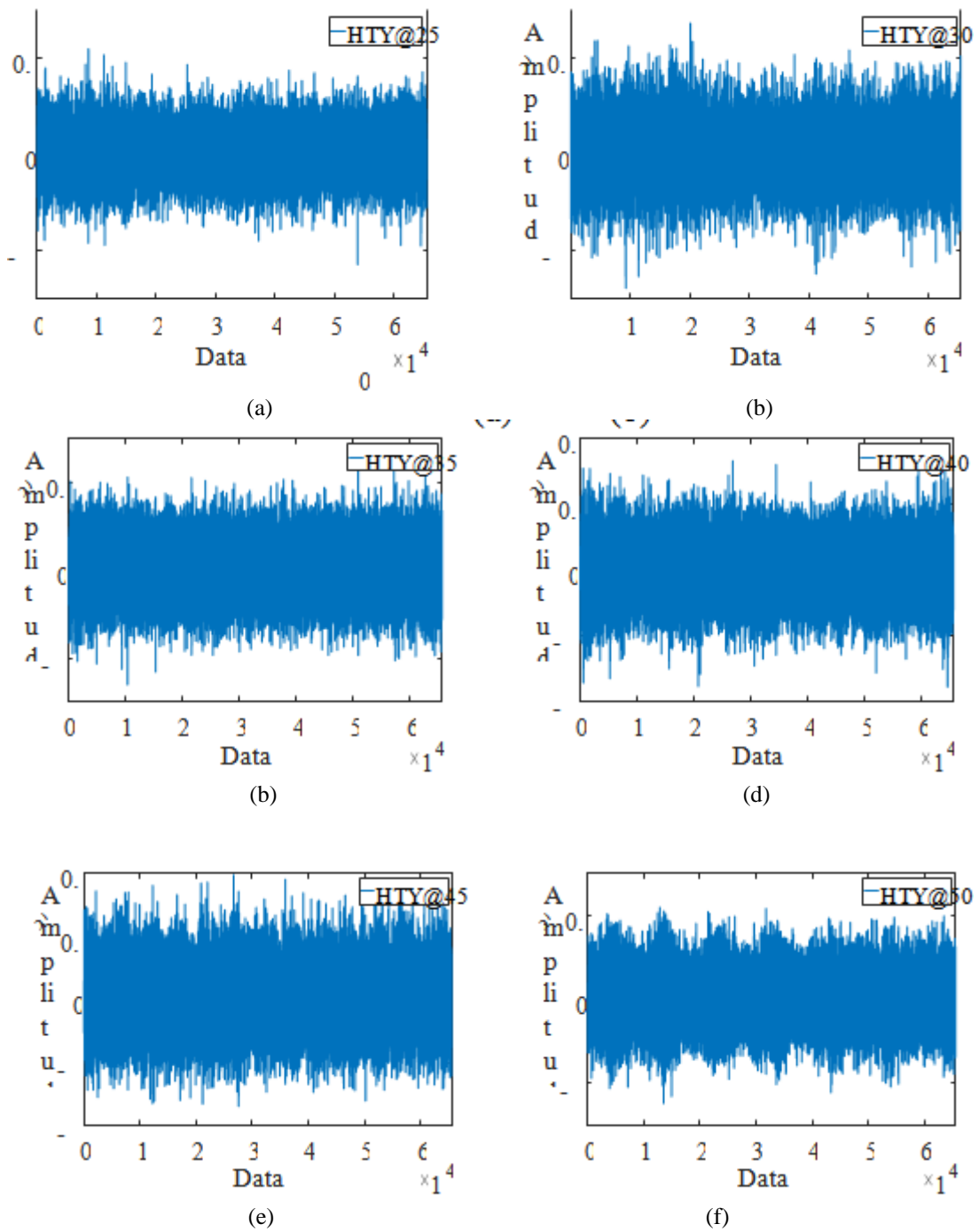


Figure 5: Time domain signals for the healthy bearing at various speeds: (a) 25Hz;(b) 30 Hz; (c) 35 Hz; (d) 40 Hz; (e) 45 Hz, and (f) 50 Hz

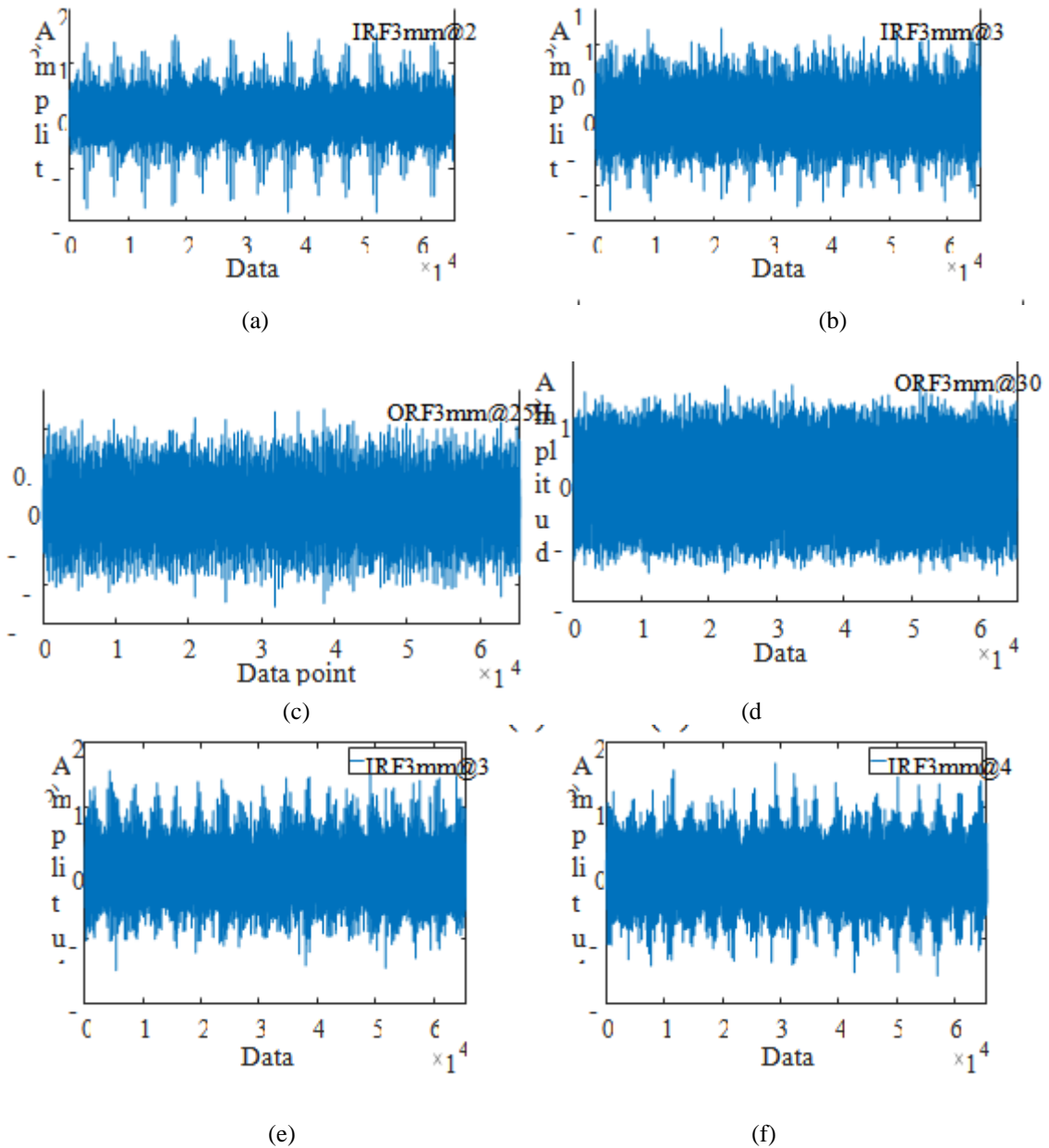


Figure 6: Time domain signals for IRF with the fault size of 3mm: (a) at 25 Hz; (b) at 30 Hz; (c) at 35 Hz; (d) at 40 Hz; (e) at 45 Hz; (f) at 50 Hz

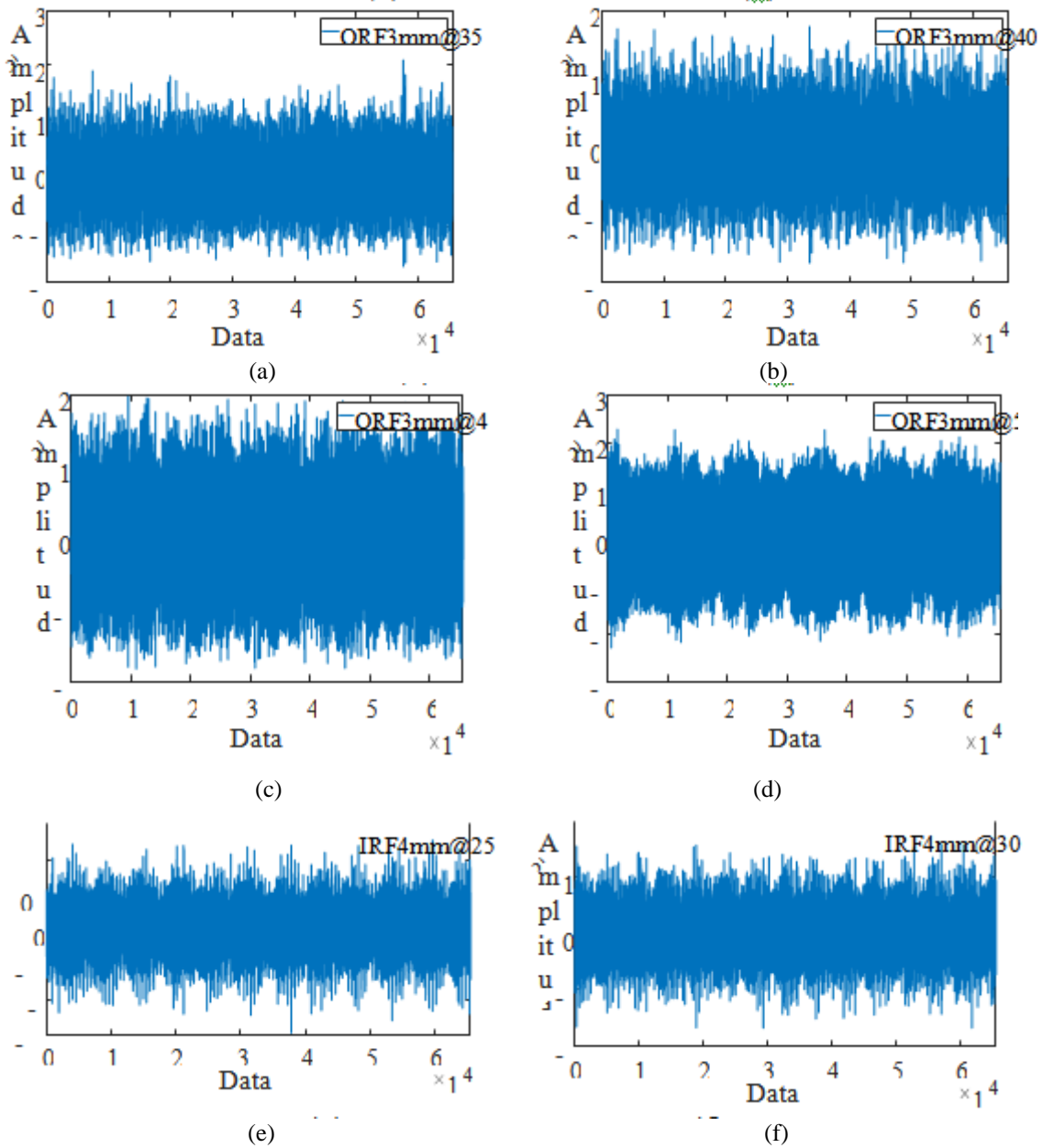


Figure 7: Time domain signals for ORF with the fault size of 3mm: (a) at 30 Hz; (b) at 40 Hz; (c) at 25 Hz; (d) at 30 Hz; (e) at 45 Hz; (f) at 50 Hz

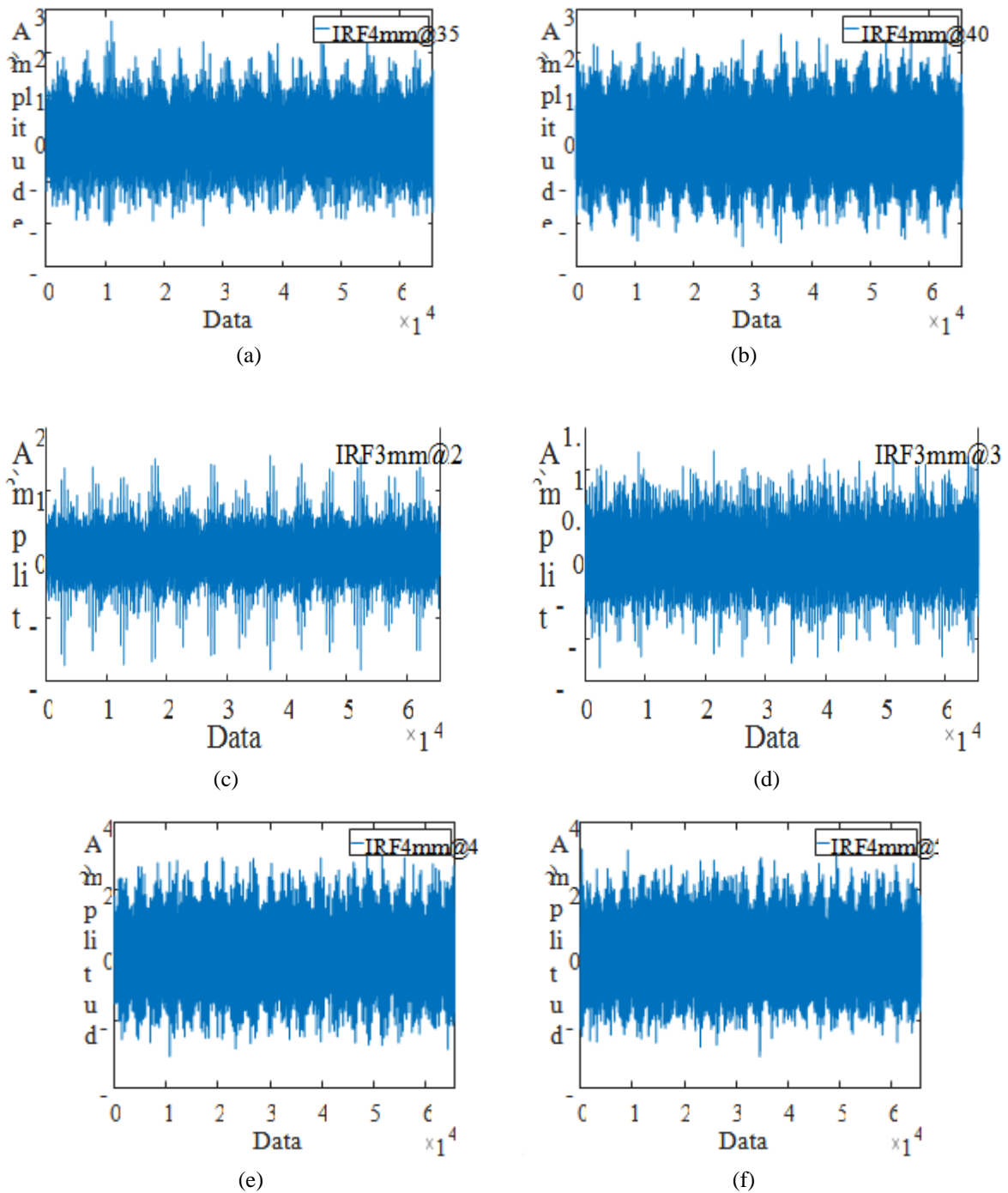


Figure 8: Time domain signals for IRF with the fault size of 4mm: (a) at 25 Hz; (b) at 30 Hz; (c) at 35 Hz; (d) at 40 Hz; (e) at 45 Hz; (f) at 50 Hz

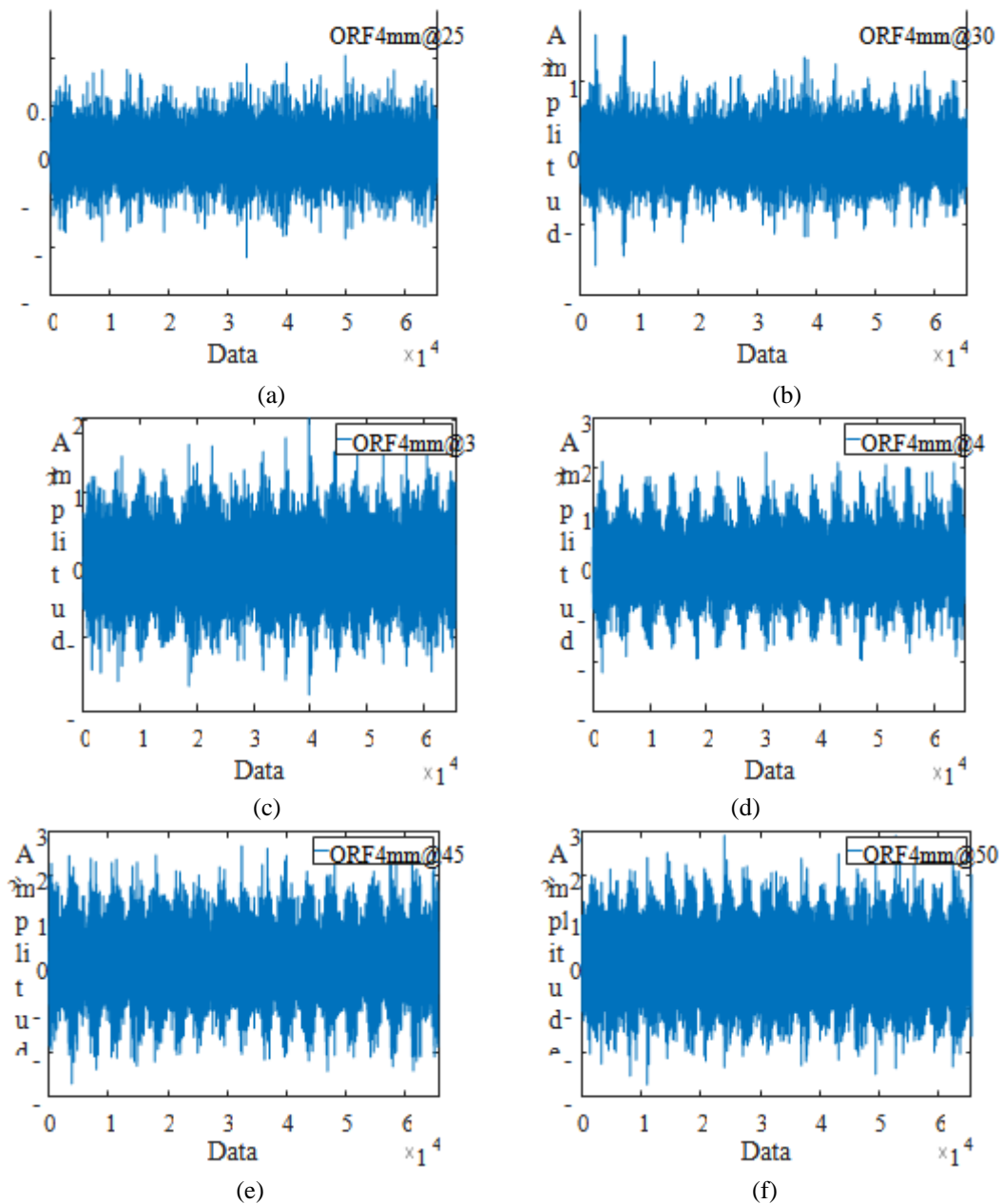


Fig. 9: Time domain signals for ORF with the fault size of 4mm: (a) at 25 Hz;(b) at 30 Hz; (c) at 35 Hz; (d) at 40 Hz; (e) at 45 Hz; (f) at 50 Hz

B. EEMD on Experimental Signal-

The acquired machine signals usually have low signal-to-noise ratio (SRN). The SRN of a signal can be enhanced by pre-processing. The pre-processors are usually the electronic filters and decomposes the signal into different sub-bands. The EMD based filters are extensively applied to decompose the acquired machine signals. Many advancement to the conventional EMD algorithm were reported time-to-time by various researchers. One such advancement is the EEMD technique, to overcome mode mixing problem and gives finer results than EMD. The

EEMD technique is a powerful tool for non-linear and non-stationary signal analysis.

Each signal reflecting different experimental conditions was first decomposed by EEMD. The decomposed sub-bands are called intrinsic mode functions (IMFs). The various parameters used for the algorithms of EEMD are:

- (i). the standard deviation of the additional noise to the standard deviation of the signal is 0.2.
- (ii). Ensemble number for the EEMD = 120.

Features extraction: In the present study five statistical and five entropy features are extracted from the residual signal. The detail of them are: Statistical features (a) Root mean square value (RMS), (b) Kurtosis (Ku), (c) Standard Deviation (SD), (d) Impulse factor (IF), (e) Peak-to-RMS (pk2rms). Entropy features (a) Approximate Entropy (ApEn), (b) Sample

Entropy (SampEn), (c) Fuzzy Entropy (FzEn), (d) Permutation Entropy (PE), (e) Dispersion Entropy (DE).

C. EEMD of signals acquired for healthy bearing
 Decomposition levels for healthy bearing at different operating speeds are given in Figure 10 (a-f).

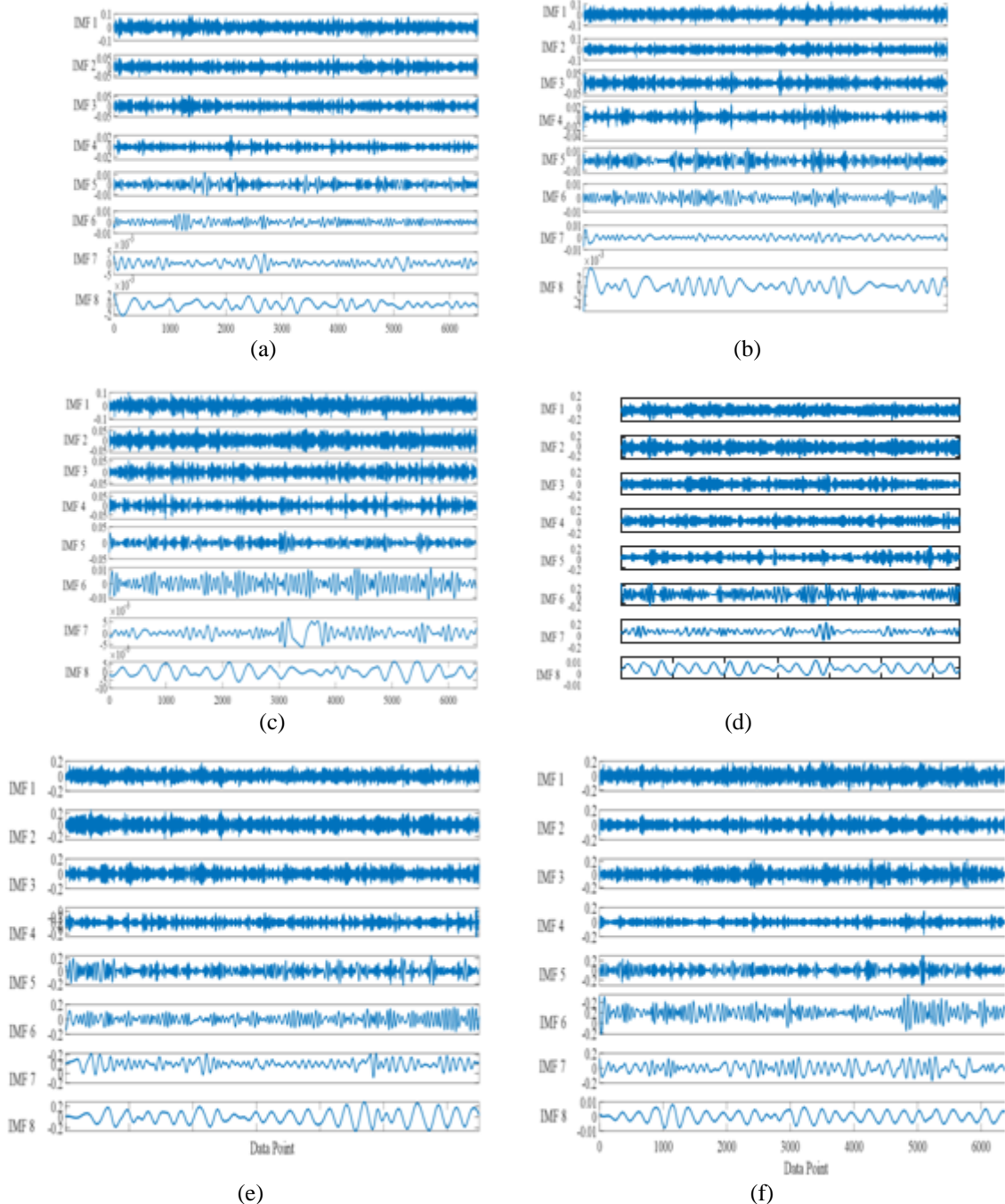
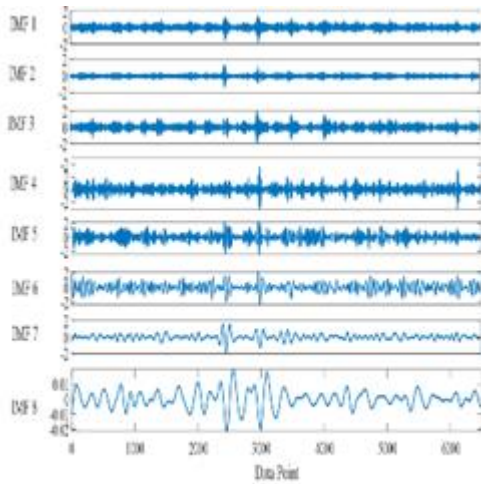


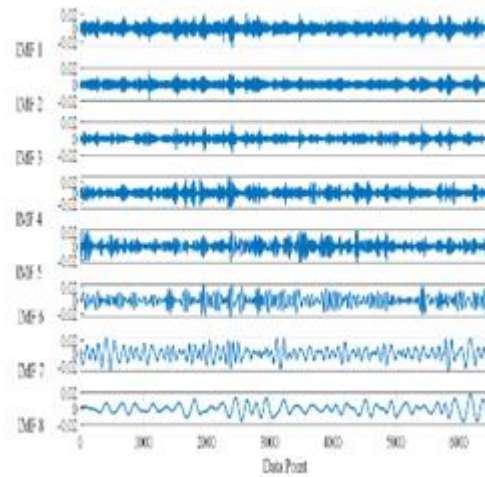
Fig.10 IMF decomposition obtained through EEMD of Healthy bearing signals:(a)25 Hz; (b) 30 Hz; (c) 35 Hz; (d) 40 Hz; (e) 45 Hz; and (f) 50 Hz

D.EEMD on signals acquired of bearings with IRF-

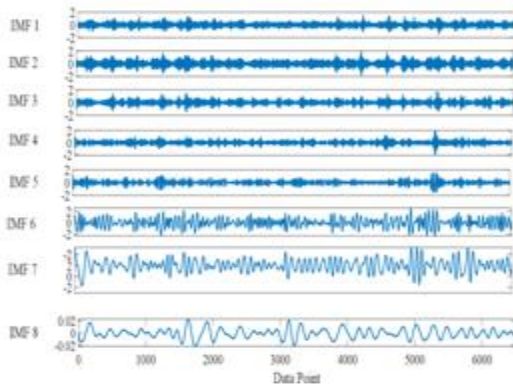
Decomposition levels of bearing with IRF, for the fault severity of 3 mm, 4mm and 5mm at different operating conditions are given in Fig 11, Fig12 and Fig.13 respectively.



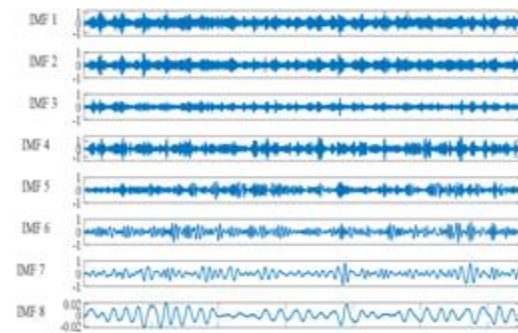
(a)



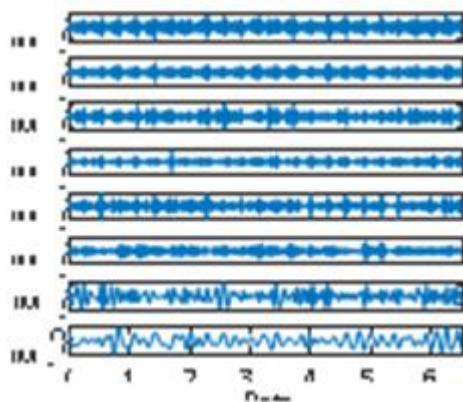
(b)



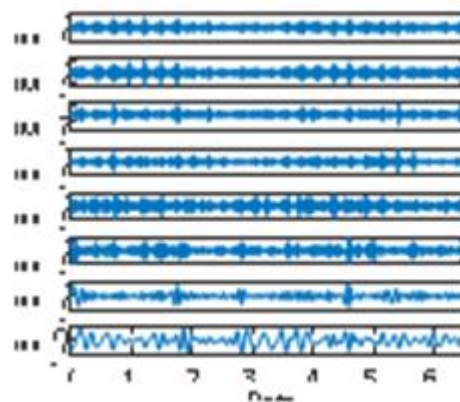
(c)



(d)



(e)



(f)

Fig. 11 IMF decomposition obtained through EEMD of bearing's with IRF of 3mm, at: (a) 25 Hz; (b) 30 Hz; (c) 35 Hz; (d) 40 Hz; (e) 45 Hz; and (f) 50 Hz

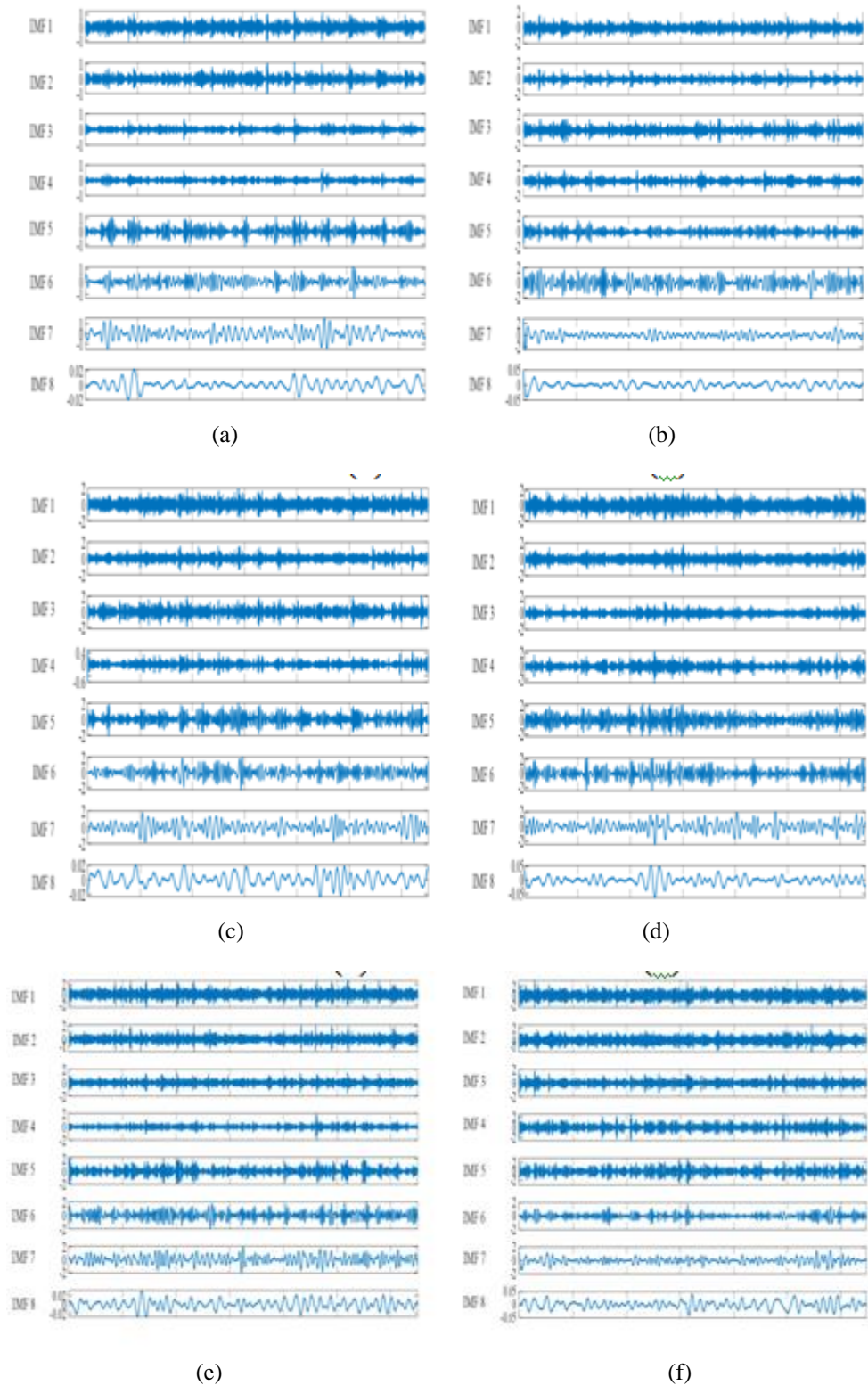


Fig.12 IMF decomposition obtained through EEMD of bearing's with IRF of 4mm, at: (a) 25 Hz; (b) 30 Hz; (c) 35 Hz; (d) 40 Hz; (e) 45 Hz; and (f) 50 Hz

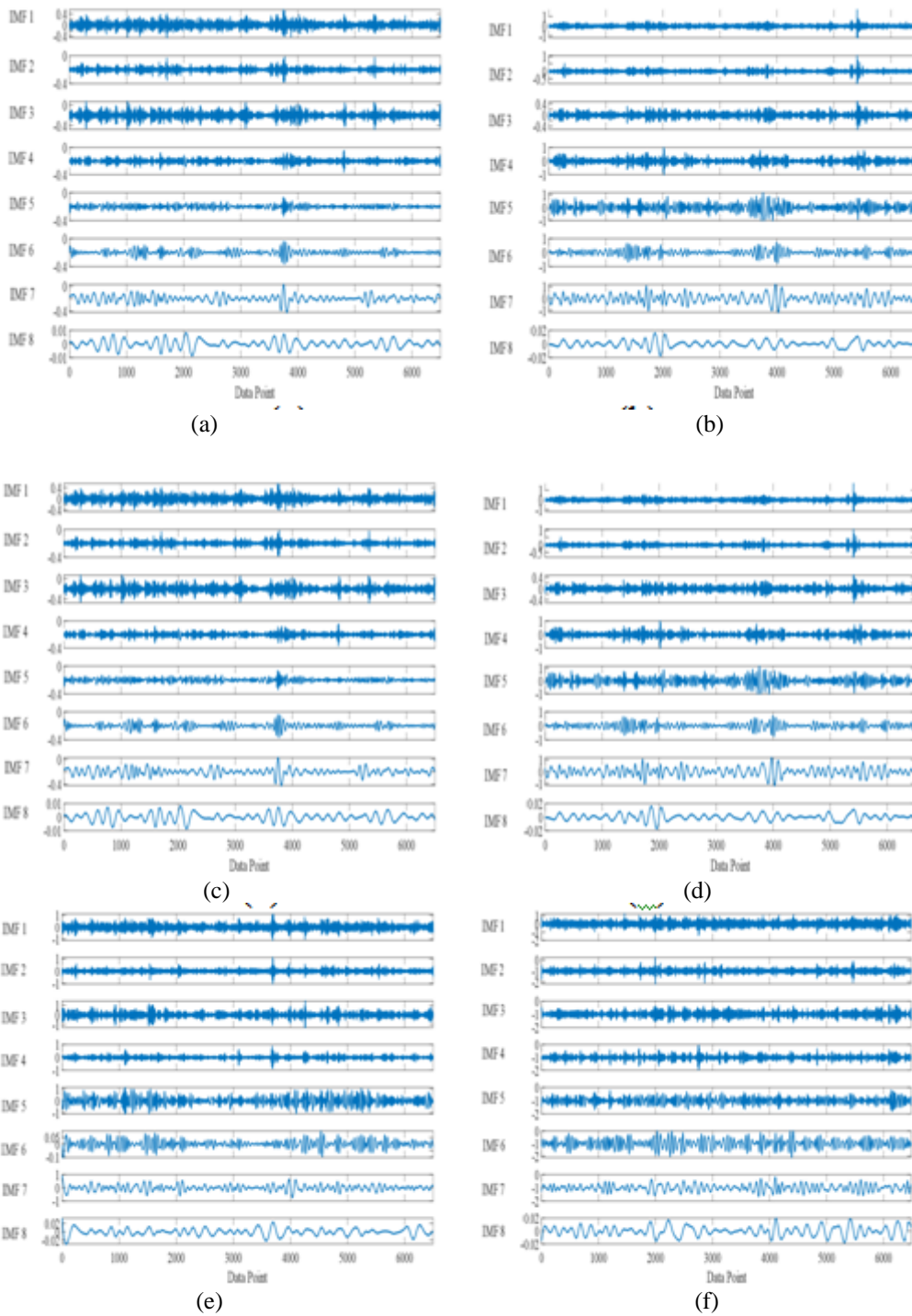


Fig. 13 IMF decomposition obtained through EEMD of bearing's with IRF of 5mm, at: (a) 25 Hz; (b) 30 Hz; (c) 35 Hz; (d) 40 Hz; (e) 45 Hz; and (f) 50 Hz

E.EEMD on signals acquired of bearings with ORF-

Decomposition levels of bearing with ORF, for the fault severity of 3 mm, 4mm and 5mm at different operating conditions are given in Fig. 14, Fig.15 and Fig.16 respectively.

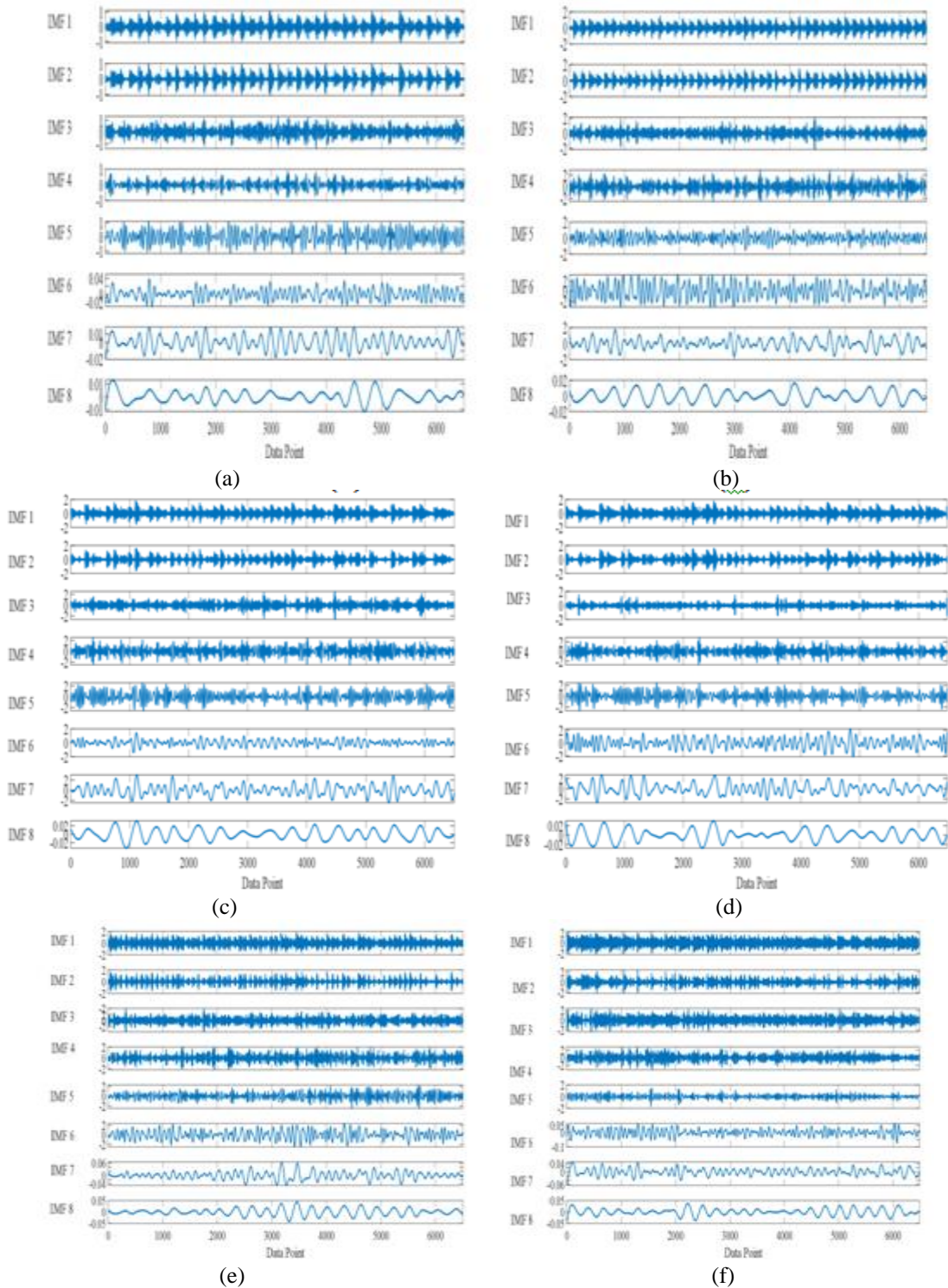


Fig. 14 IMF decomposition obtained through EEMD of bearing's with ORF of 3mm, at: (a) 25 Hz; (b) 30 Hz; (c) 35 Hz; (d) 40 Hz; (e) 45 Hz; and (f) 50 Hz

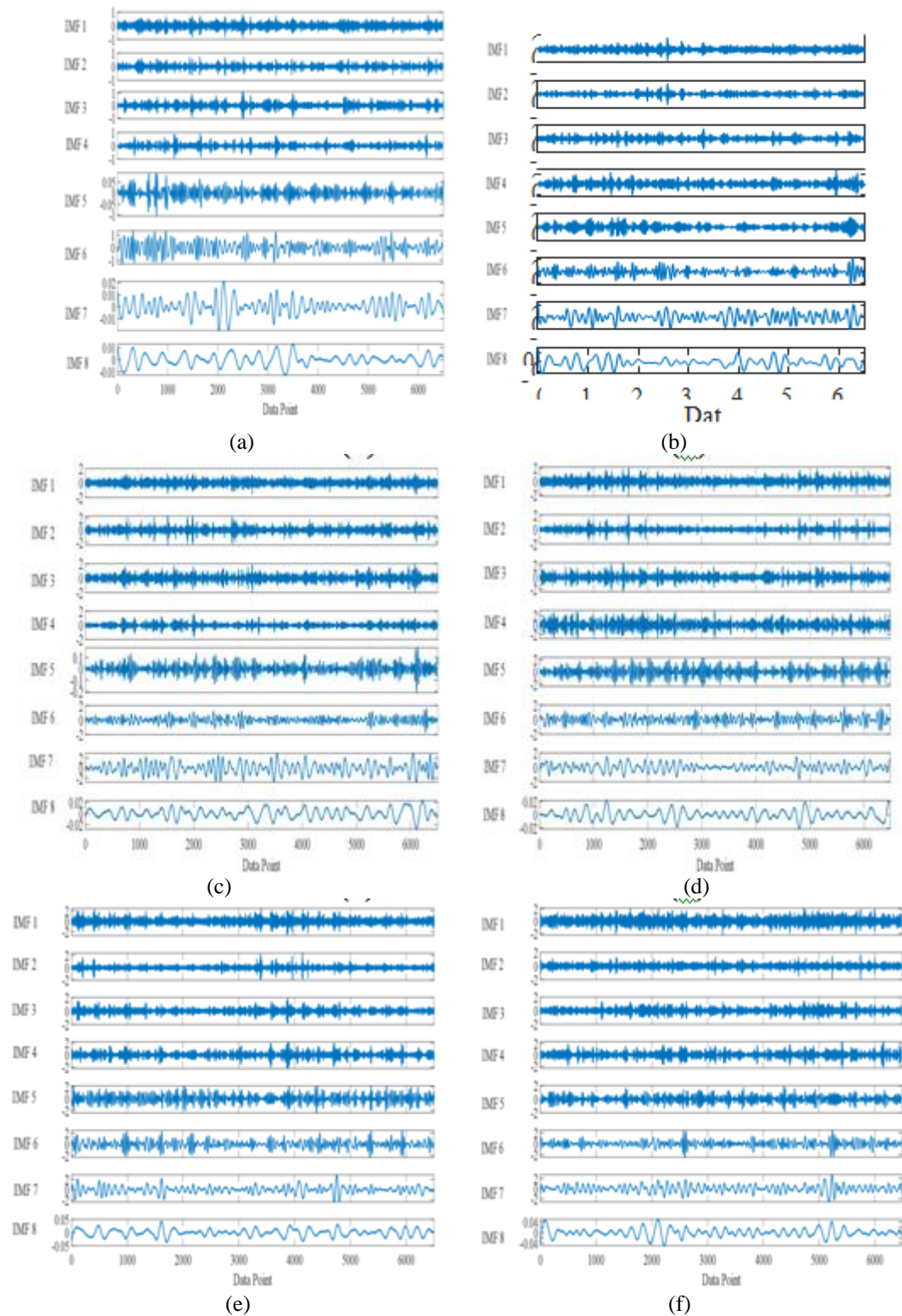


Fig. 15 IMF decomposition obtained through EEMD of bearing's with ORF of 4mm, at: (a) 25 Hz; (b) 30 Hz; (c) 35 Hz; (d) 40 Hz; (e) 45 Hz; and (f) 50 Hz

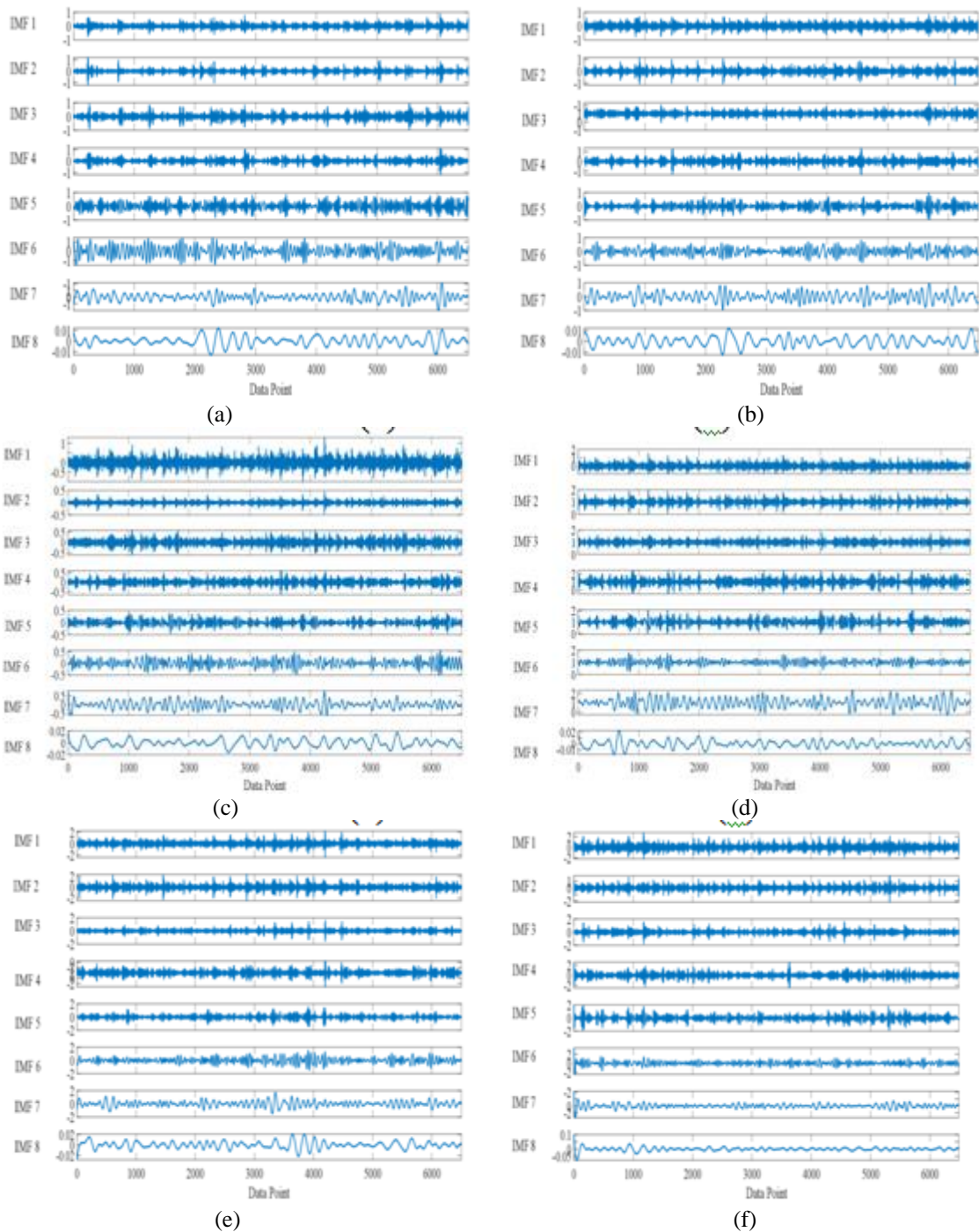


Fig. 16 IMF decomposition obtained through EEMD of bearing's with ORF of 5mm, at: (a) 25 Hz; (b) 30 Hz; (c) 35 Hz; (d) 40 Hz; (e) 45 Hz; and (f) 50 Hz

In the present study, the residual signals are obtained by subtracting the sum of insignificant IMFs from the original signals. The selection of significant IMFs is based upon their similarity index obtained using DTW algorithm. Five-statistical and five entropy features are extracted as the input features. These features are used to train and test two

classifiers based on “support vector machine (SVM) and random forest (RF)” to detect the fault type in the bearing.
 $R(t) = x(t) - \text{sum}(\text{insignificant IMFs})$ (1)
 The statistical and entropy-based feature values for the residual signal of healthy bearing, acquired at different speeds, are computed and tabulated. Table 2 can be referred for



statistical feature values of healthy bearing running at different speeds. The values of different entropy-based features, calculated at different operating conditions can be observed from Table.4

Table- 4 Statistical features: Extracted from EEMD based residual signal of healthy bearing

| Bearing condition | Feature vector | Speed | | | | | |
|-------------------|----------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| HTY | <i>RMS</i> | 0.0703 | 0.0784 | 1.4761 | 3.2491 | 3.9743 | 3.1684 |
| | <i>Ku</i> | 2.0369 | 2.0354 | 2.9803 | 3.0461 | 3.0938 | 3.0067 |
| | <i>IF</i> | 0.0270 | 0.0270 | 5.0465 | 5.4429 | 4.0796 | 4.0675 |
| | <i>SD</i> | 0.0349 | 0.0349 | 5.6266 | 4.7894 | 4.9605 | 5.0256 |
| | <i>pk2rms</i> | 0.0198 | 0.0163 | 3.6021 | 4.8367 | 3.8161 | 3.5634 |

Table- 5: Entropy features: Extracted from EEMD based residual signal of healthy bearing

| Bearing condition | Feature vector | Speed | | | | | |
|-------------------|----------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| HTY | <i>ApEn</i> | 0.0122 | 0.0343 | 0.7684 | 0.7876 | 0.9553 | 0.9893 |
| | <i>SampEn</i> | 1.3206 | 2.6580 | 2.6748 | 2.9847 | 2.9957 | 2.8974 |
| | <i>FzEn</i> | 0.2267 | 0.6743 | 4.7664 | 5.0006 | 4.9963 | 4.8746 |
| | <i>PE</i> | 2.9958 | 2.8956 | 3.9967 | 3.7894 | 3.0001 | 3.9887 |
| | <i>DE</i> | 1.1078 | 1.5012 | 2.9711 | 2.8858 | 2.9012 | 2.8947 |

After extracting the statistical and entropy features from the residual signal of healthy bearing at different speeds, the feature extraction is done for the bearings with inner race faults. The both statistical and entropy-based features were extracted for different types of IRFs at different operating

conditions. The values of the different statistical and Entropy features obtained for the fault size of 3mm, 4mm and 5mm, are tabulated in Table 4, Table 5, Table 6, Table7, Table8 and Table 9 respectively.

| Bearing condition | Feature vector | Speed | | | | | |
|-------------------|----------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| IRF (3 mm) | <i>RMS</i> | 1.4879 | 2.6034 | 4.0143 | 4.5863 | 5.0066 | 5.9403 |
| | <i>Ku</i> | 5.9875 | 6.0034 | 7.9001 | 7.6687 | 6.9889 | 7.9976 |
| | <i>IF</i> | 3.2176 | 3.8791 | 5.0997 | 5.9044 | 6.1117 | 6.7836 |
| | <i>SD</i> | 3.7893 | 3.6988 | 5.7743 | 6.7894 | 7.5069 | 8.6725 |
| | <i>pk2rms</i> | 3.8235 | 3.8965 | 4.6654 | 5.8777 | 6.1234 | 5.9054 |

Table-6 Statistical features: Extracted from EEMD based residual signal of bearing with IRF (for the fault severity of 3 mm) at different speeds



| Bearing condition | Feature | Speed | | | | | |
|-------------------|---------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| IRF (4mm) | <i>RMS</i> | 2.3370 | 4.9874 | 5.3678 | 6.0021 | 6.7453 | 7.8711 |
| | <i>Ku</i> | 2.5646 | 2.7856 | 4.6540 | 6.7776 | 7.5465 | 8.6232 |
| | <i>IF</i> | 1.6671 | 1.4720 | 4.7845 | 5.7721 | 4.9990 | 4.5799 |
| | <i>SD</i> | 4.7856 | 6.1511 | 6.5655 | 7.0023 | 7.1237 | 8.8895 |
| | <i>pk2rms</i> | 4.6730 | 4.0300 | 5.3146 | 4.6692 | 4.6649 | 4.5571 |

Table-7 Statistical features: Extracted from EEMD based residual signal of bearing with IRF (for the fault severity of 4 mm) at different speeds

| Bearing condition | Feature | Speed | | | | | |
|-------------------|---------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| IRF (5 mm) | <i>RMS</i> | 5.7056 | 6.8890 | 9.8978 | 8.6645 | 9.0067 | 9.5677 |
| | <i>Ku</i> | 7.8865 | 8.0062 | 8.9886 | 9.4589 | 9.1123 | 9.1008 |
| | <i>IF</i> | 1.1342 | 2.0010 | 5.5675 | 5.6675 | 6.1157 | 6.8815 |
| | <i>SD</i> | 3.4562 | 3.0034 | 5.1254 | 6.7781 | 6.7321 | 7.7659 |
| | <i>pk2rms</i> | 3.4451 | 4.5567 | 5.8757 | 4.1259 | 4.8278 | 4.7590 |

Table-8: Statistical features: Extracted from EEMD based residual signal of bearing with IRF (for the fault severity of 5 mm) at different speeds

| Bearing condition | Feature | Speed | | | | | |
|-------------------|---------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| IRF (3 mm) | <i>ApEn</i> | 0.6574 | 0.7075 | 0.7689 | 0.8237 | 0.9758 | 0.9995 |
| | <i>SampEn</i> | 3.7904 | 3.7566 | 4.8764 | 4.9993 | 5.9037 | 5.8865 |
| | <i>FzEn</i> | 1.7745 | 1.8761 | 4.9984 | 6.9073 | 6.9878 | 7.5763 |
| | <i>PE</i> | 4.3876 | 4.9986 | 7.0043 | 6.8967 | 7.1298 | 7.9762 |
| | <i>DE</i> | 3.3345 | 3.1205 | 4.9865 | 5.9876 | 5.7756 | 6.8790 |

Statistical and entropy-based features were extracted for different types of ORFs at different operating conditions. The values of the different statistical and entropy features obtained

for the fault size of 3mm, 4mm and 5mm, are tabulated in Table 10, Table 11, Table 12, Table13, Table14 and Table 15, respectively.

Table-9 Entropy features: Extracted from EEMD based residual signal of bearing with IRF (for the fault severity of 5 mm) at different speeds

| Bearing condition | Feature vector | Speed | | | | | |
|-------------------|----------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| ORF (3 mm) | <i>RMS</i> | 2.1035 | 2.5569 | 3.7839 | 5.8743 | 6.4598 | 7.7782 |
| | <i>Ku</i> | 5.6743 | 6.5603 | 7.1456 | 7.9754 | 9.2940 | 9.4006 |
| | <i>IF</i> | 4.5535 | 4.3070 | 4.8665 | 4.7789 | 7.4451 | 7.5476 |
| | <i>SD</i> | 3.2398 | 3.5582 | 5.9751 | 6.7845 | 7.0094 | 7.8965 |
| | <i>pk2rms</i> | 4.0331 | 4.9301 | 4.1111 | 5.7825 | 6.0048 | 7.8954 |

Table -10: Statistical features: Extracted from EEMD based residual signal of bearing with ORF (for the fault severity of 3 mm) at different speeds

| Bearing condition | Feature vector | Speed | | | | | |
|-------------------|----------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| ORF (4mm) | <i>RMS</i> | 4.4589 | 4.8540 | 5.5948 | 7.1231 | 7.0080 | 7.9841 |
| | <i>Ku</i> | 3.1104 | 3.6548 | 4.8814 | 6.6593 | 7.0049 | 8.9975 |
| | <i>IF</i> | 2.9452 | 3.1231 | 4.5569 | 4.9867 | 5.0076 | 5.3256 |
| | <i>SD</i> | 5.9854 | 6.4872 | 7.8353 | 8.4671 | 8.1263 | 8.0009 |
| | <i>pk2rms</i> | 5.1190 | 5.0500 | 5.5111 | 5.5464 | 5.0830 | 6.6784 |

Table -11: Statistical features: Extracted from EEMD based residual signal of bearing with ORF (for the fault severity of 4 mm) at different speeds

| Bearing condition | Feature vector | Speed | | | | | |
|-------------------|----------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| ORF (5 mm) | <i>RMS</i> | 6.8874 | 6.7804 | 9.0112 | 9.0003 | 9.5431 | 9.9987 |
| | <i>Ku</i> | 8.8978 | 8.7624 | 8.8769 | 9.3986 | 9.2276 | 9.7839 |
| | <i>IF</i> | 2.3568 | 2.9836 | 5.8793 | 5.9982 | 6.8673 | 7.0108 |
| | <i>SD</i> | 4.6521 | 4.5756 | 5.6573 | 5.9006 | 6.9981 | 8.6705 |
| | <i>pk2rms</i> | 5.6742 | 5.5678 | 6.4034 | 6.7780 | 6.1450 | 6.9003 |

Table- 12: Statistical features: Extracted from EEMD based residual signal of bearing with ORF (for the fault severity of 5 mm) at different speeds

| Bearing condition | Feature vector | Speed | | | | | |
|-------------------|----------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| ORF (3 mm) | <i>ApEn</i> | 0.7543 | 0.7869 | 0.9659 | 0.9093 | 0.9652 | 0.9767 |
| | <i>SampEn</i> | 3.6654 | 3.9063 | 5.6211 | 6.0099 | 6.6078 | 6.9004 |
| | <i>FzEn</i> | 3.6759 | 4.0179 | 4.4467 | 5.6303 | 5.9076 | 5.0950 |
| | <i>PE</i> | 2.2008 | 2.4405 | 3.1108 | 3.2085 | 3.9573 | 4.0405 |
| | <i>DE</i> | 6.0039 | 6.0491 | 5.9909 | 7.9067 | 7.9111 | 7.8460 |

Table 13: Entropy features: Extracted from EEMD based residual signal of bearing with ORF (for the fault severity of 3 mm) at different speeds

| Bearing condition | Feature vector | Speed | | | | | |
|-------------------|----------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| ORF (4mm) | <i>RMS</i> | 4.4589 | 4.8540 | 5.5948 | 7.1231 | 7.0080 | 7.9841 |
| | <i>Ku</i> | 3.1104 | 3.6548 | 4.8814 | 6.6593 | 7.0049 | 8.9975 |
| | <i>IF</i> | 2.9452 | 3.1231 | 4.5569 | 4.9867 | 5.0076 | 5.3256 |
| | <i>SD</i> | 5.9854 | 6.4872 | 7.8353 | 8.4671 | 8.1263 | 8.0009 |
| | <i>pk2rms</i> | 5.1190 | 5.0500 | 5.5111 | 5.5464 | 5.0830 | 6.6784 |

Table 14: Entropy features: Extracted from EEMD based residual signal of bearing with ORF (for the fault severity of 4 mm) at different speeds

| Bearing condition | Feature vector | Speed | | | | | |
|-------------------|----------------|--------|--------|--------|--------|--------|--------|
| | | 25Hz | 30Hz | 35Hz | 40Hz | 45Hz | 50Hz |
| ORF (5 mm) | <i>ApEn</i> | 0.8967 | 0.8978 | 0.9954 | 0.9817 | 0.9899 | 0.9877 |
| | <i>SampEn</i> | 3.3435 | 3.5670 | 6.6741 | 7.1457 | 7.8506 | 7.9804 |
| | <i>FzEn</i> | 3.5645 | 3.5611 | 4.9867 | 5.7141 | 6.6458 | 6.8745 |
| | <i>PE</i> | 2.9096 | 2.9984 | 3.7060 | 3.0718 | 3.8891 | 5.6785 |
| | <i>DE</i> | 6.7083 | 7.8650 | 9.4795 | 9.5601 | 9.1239 | 8.9564 |

Two types of bearing faults with different degree of damage were considered in the present study: Inner race fault, outer race fault. For each type of fault, its size was varied from 3 mm to 5 mm with an intermittent fault size of 4 mm.

For Group-I, the features for healthy bearings and IRFs with various degrees of damage at various speeds were considered.

Thus Group-I contain 60 features extracted from the residual signal of healthy bearing and 180 features extracted from the bearings with IRF damages. Total number of features in Group-I is thus 240. Table 16 show the accuracy obtained with both of the classifiers.



For Group-II, the data for healthy bearing (60 features) and ORFs (180 features) with various degrees of damage at various speeds were considered. Table 17 show the accuracy with both the machine learning tools.
 For Group-III, the data for IRFs (180 features) and ORFs (180 features) with various degrees of damage at various speeds

were considered. Table 18 show the accuracy with both the classifiers.
 For Group-IV, the data for healthy bearing (60 features), IRFs (180 features), and ORFs (180 features) with various degrees of damage at various speeds were considered. Table 19 show the accuracy with both the classifiers.

Table -15 Groups for classification ('√' included data and '-' data not included)

| Group number | Type of data | | |
|--------------|--------------|-----|-----|
| | HTY | IRF | ORF |
| G-I | √ | √ | - |
| G-II | √ | - | √ |
| G-III | - | √ | √ |
| G-IV | √ | √ | √ |

Table- 16: Classification accuracy for Group I

| Group Number | Total samples | Tested samples | Accuracy | |
|--------------|---------------|----------------|----------|----|
| | | | SVM | RF |
| G-I | 240 | 96 | 95 | 96 |

Table- 17 Classification accuracy for Group II

| Group Number | Total samples | Tested samples | Accuracy | |
|--------------|---------------|----------------|----------|----|
| | | | SVM | RF |
| G-II | 240 | 96 | 97 | 98 |

Table -18 Classification accuracy for Group III

| Group Number | Total samples | Tested samples | Accuracy | |
|--------------|---------------|----------------|----------|----|
| | | | SVM | RF |
| G-III | 360 | 144 | 98 | 98 |

Table -19 Classification accuracy for Group IV

| Group Number | Total samples | Tested samples | Accuracy | |
|--------------|---------------|----------------|----------|----|
| | | | SVM | RF |
| G-IV | 420 | 168 | 99 | 98 |

V. CONCLUSION

Based on ensemble empirical mode decomposition (EEMD) residual signals, this study presents an effective method for fault detection in the roller bearings. In the present study, the EEMD is used to pre-process the acquired bearing vibration signals. The sensitive intrinsic mode functions (IMFs) are selected on the basis of their similarity index value computed by applying the dynamic time wrapping algorithm. The bearing health conditions are then identified using five statistical and five entropy based features extracted from the residual signal and fed into two state-of-the-art classifiers, “support vector machine (SVM) and random forest (RF)”. The results of the diagnosis show that the proposed method is capable of reliably identifying various types of bearing defects. It can be stated that EEMD based residual signals can be used to achieve a good fault recognition accuracy. It accurately detects the various sorts of bearing defects.

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