COMPARATIVE STUDY OF DIFFERENT TRANSFORMERLESS BUCK-BOOST CONVERTERS

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Abstract—A comparative study of different buck-boost converters is aimed in this paper. The traditional buck-boost converter and KY buck-boost converter are compared with the new transformerless buck-boost converter. The new transformerless buck-boost converter's voltage gain is squared times that of the former and its output voltage polarity is positive. The two power switches of the new transformerless buck-boost converter operate synchronously. These advantages enable it to work in a wider range of positive output voltage. The output voltages for different duty ratios for new transformerless buck-boost converter are compared with the other two buck-boost converters. They are also compared for their efficiencies. The simulations of these buck-boost converters are done using MATLAB/SIMULINK software. The hardware of the new transformerless buck-boost converter is also made. The control circuit is implemented using PIC16F877A.

Keywords— Buck-boost converter, KY converter

I. INTRODUCTION

Owing to energy crisis and global warming, Green energy is attracting more and more attention, resulting in the demand for the green energy, which produces less pollution on the environment. The green energy facilities include wind power, solar cells, fuel cells and so on. In many applications, because the above mentioned green energy facilities suffer from unstable and lower output voltages, high-voltage conversion converters play an important role in maintaining the output voltage at a constant value and boosting the low output voltages of the green power facilities to the high voltages which the loads need. For example, the traditional fuel cell system in a vehicle boosts 12V to 48V or 72V or more to drive the LED loads, the heating fans, sound system equipment and so on. Regarding the traditional non-isolated voltage-boosting converters, such as the traditional boost converter and the buck-boost converter, their voltage gains are not high enough. Many applications require voltage bucking/boosting converters, such as portable devices, car electronic devices, etc. This is because the battery has quite large variations in output voltage, and hence, the additional switching power supply is indispensable for processing the varied input voltage so as to generate the stabilized output voltage. A KY converter uses four switches. In order to reduce the number of power switches in KY converter, the KY converter and the SR buck converter, combined into a buck-boost converter, i.e., KY buck-boost converter or 2D converter, both use the same power switches. By inserting an additional switched network into the traditional buck-boost converter, a new transformerless buck-boost converter is presented. The main merit of this new transformerless buck-boost converter is that its voltage gain is quadratic of the traditional buck-boost converter so that it can operate in a wide range of output voltage. Here we will compare the new transformerless buck-boost converter with traditional buck-boost converter and KY buck-boost converter for their performance.

II. WORKING

A. Traditional Buck-Boost Converter

Traditional buck boost converter is the simplest buck-boost converter. Working of traditional buck-boost converter is shown in the Fig.1. When switch S is ON, inductor gets charged and the diode is reverse biased. When switch S is OFF, the energy stored in the inductor is transferred to the output. No energy is transferred by the input during this interval.
A typical buck-boost converter, which combines two converters using the same power switches is shown in Fig. 2. One is the SR buck converter, which is built up by two power switches $S_1$ and $S_2$, one inductor $L_1$, one energy-transferring capacitor $C_1$, whereas the other is the KY converter, which is constructed by two power switches $S_1$ and $S_2$, one power diode $D$, which is disconnected from the input voltage source and connected to the output of the SR buck converter, one energy-transferring capacitor $C_2$, one output inductor $L_2$, and one output capacitor $C_0$. The output load is signified by $R$. Furthermore, during the magnetization period, the input voltage of the KY converter is supplied by the input voltage source, whereas during the demagnetization period, the input voltage of the KY converter is supplied from output voltage of the SR buck converter. In addition, during the startup period with $S_1$ ON and $S_2$ OFF, the inductors $L_1$ and $L_2$ are both magnetized. At the same time, $C_1$ is charged, and so, the voltage across $C_1$ is positive, whereas $C_2$ is reverse charged, and hence, the voltage across $C_2$ is negative. Sequentially, during the startup period with $S_1$ OFF and $S_2$ ON, inductors $L_1$ and $L_2$ are both demagnetized. At the same time, $C_1$ is discharged. Since $C_2$ is connected in parallel with $C_1$, $C_2$ is reverse charged with the voltage across $C_2$ being from negative to positive, and finally, the voltage across $C_2$ is the same as the voltage across $C_1$.

In Continuous Conduction Mode (CCM), there are two modes of operation, that is, mode 1 and mode 2, in the new transformerless buck-boost converter.

a) Mode 1: $NT < t < (N+D)T$

In this mode, the switches $S_1$ and $S_2$ are turned on, while $D_1$ and $D_0$ are reverse biased. It is seen that $L_1$ is magnetized from the input supply $V_{in}$ while $L_2$ is magnetized from $V_{in}$ and capacitor $C_1$. This is shown in Fig.4. This time, the output is supplied by the output capacitor $C_0$. Thus, the corresponding equations can be established as:

$$V_{L_1} = V_{in}$$

$$V_{L_2} = V_{in} + V_{C_1}$$

C. New Transformerless Buck-Boost Converter

New Transformerless Buck-Boost Converter consists of two power switches ($S_1$ and $S_2$), two diodes ($D_1$ and $D_0$), two inductors ($L_1$ and $L_2$), two capacitors ($C_1$ and $C_0$) and one resistive load (R) is shown in Fig. 3. Power switches $S_1$ and $S_2$ are controlled synchronously. When the power switches $S_1$ and $S_2$ are turned ON, the diodes $D_1$ and $D_0$ do not conduct. At this instant both the inductors $L_1$ and $L_2$ are magnetized, and the charge pump capacitor $C_1$ and the output capacitor $C_0$ are discharged. When the power switches $S_1$ and $S_2$ are turned OFF, the diodes $D_1$ and $D_0$ conduct for its and hence both the inductors $L_1$ and $L_2$ are demagnetized, and both the capacitors $C_1$ and $C_0$ are charged. Here we assumed that the converter operates in steady state, all components are ideal, and all capacitors are large enough to keep the voltage across them constant.
Fig. 5. Theoretical waveforms of the converter in Mode 1 operation

b) Mode 2: \((N+D)T < t < (N+1)T\)

In mode 2, the switches \(S_1\) and \(S_2\) are turned off, while \(D_1\) and \(D_0\) are forward biased. It is seen that the energy stored in the inductor \(L_1\) is released to the capacitor \(C_1\) via the diode \(D_1\). At the same time, the energy stored in the inductor \(L_2\) is released to the capacitor \(C_1\), the output capacitor \(C_0\) and the resistive load \(R\) through the diodes \(D_0\) and \(D_1\). The equations of the mode 2 are described as follows:

\[
V_{L1} = -V_{C1}
\]  
\[
V_{L2} = -(V_{C1} + V_0)
\]

Fig. 6. Circuit of the New Transformerless buck-boost converter in Mode 2

Fig. 6. Theoretical waveforms of the converter in Mode 2 operation

III. SIMULATION MODEL AND RESULTS

A. Traditional Buck-Boost Converter

Traditional Buck-Boost converter is simulated in MATLAB/SIMULINK as shown in the Fig. 7.

This converter can step up the input voltage when the duty ratio is bigger than 0.5, and step down the input voltage when the duty ratio is smaller than 0.5.

The simulation results for a duty ratio of 0.6 (i.e., Step Up mode) is shown in the following Fig. 8.
When an input voltage of 18V is applied with a duty ratio of 0.6, it produced an output voltage of -26V with a switching stress of 45V.

The simulation results for a duty ratio of 0.4 (ie, Step down mode) is shown in Fig. 9.

When an input voltage of 18V is applied with a duty ratio of 0.4, the traditional buck-boost converter produced an output voltage of -11V with a switching stress of 30V.

### B. KY Buck-Boost Converter

KY Buck-Boost converter is simulated in MATLAB/SIMULINK is shown in the Fig. 10.

The simulation results for a duty ratio of 0.6 (ie, Step Up mode) is shown in the following Fig.11 and Fig.12.

![Simulink model of KY Buck-Boost converter](image)

Fig. 10. Simulink model of KY Buck-Boost converter

![Simulink result](image)

Fig. 8. Simulink result (a) Input Voltage($V_{in}$), (b) Output Voltage($V_{o}$) and (c) Switching Stress

Fig. 9. Simulink result (a) Input Voltage($V_{in}$), (b) Output Voltage($V_{o}$) and (c) Switching Stress($V_s$)

The simulation results for a duty ratio of 0.4 (ie, Step down mode) is shown in the following Fig.13 and Fig.14.

![Simulink result](image)

Fig. 11. Simulink result (a)Input Voltage($V_{in}$) and (b)Output Voltage($V_{o}$)

![Simulink result](image)

Fig. 12. Simulink result (a) Gate Pulse for $S_1$, (b) Gate Pulse for $S_2$, (c) Switch1 Stress and (d) Switch2 Stress

![Simulink result](image)

Fig. 13. Simulink result (a) Input Voltage($V_{in}$) and (b) Output Voltage($V_{o}$)
From the simulation result it can be inferred that the voltage gain of KY buckboost converter is less than the traditional buck boost converter but has the advantage that the switching stress of this converter is very less and is independent of duty cycle.

C. New Transformerless Buck-Boost Converter

The New Transformerless Buck-Boost converter of Fig. 3 is simulated in MATLAB/SIMULINK by choosing the parameters listed in Table 1 and simulink model is shown in the Fig.15.

<table>
<thead>
<tr>
<th>Table 1: Simulation Parameters</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input Voltage, ( V_{in} )</td>
</tr>
<tr>
<td>Inductor, ( L_1 )</td>
</tr>
<tr>
<td>( L_2 )</td>
</tr>
<tr>
<td>Capacitor, ( C_0 )</td>
</tr>
<tr>
<td>( C_1 )</td>
</tr>
<tr>
<td>Resistor, ( R )</td>
</tr>
<tr>
<td>Duty Ratio, ( D )</td>
</tr>
<tr>
<td>Switching frequency, ( f_s )</td>
</tr>
</tbody>
</table>

It is observed that the charge pump capacitor voltage \( V_{C1} \) is within (25.8V, 27.8V), the output voltage \( V_o \) is within (39.6V, 40.3V), the inductor current \( i_{L1} \) is within (0.7A, 1.21A), and the inductor current \( i_{L2} \) is within (0.4A, 0.80A). Also, the ripples of the inductor current \( \Delta i_{L2} \) and the inductor current \( \Delta i_{L2} \) are 0.54A and 0.45A, respectively. It is also observed that a duty ratio of up to 0.6 is suitable for this converter owing to the voltage stress across the switches.
The simulation results for a duty ratio of 0.4 (i.e., Step down mode) is shown in the Fig. 19, Fig. 20 and Fig. 21.

![Fig. 19. Simulink result (a) Input Voltage($V_{in}$) and (b) Output Voltage($V_o$)](image)

![Fig. 20. Simulink result (a) Input Current, (b) Inductor $L_2$ Current and (c) Inductor $L_1$ Current](image)

![Fig. 21. Simulink result (a) Gate Pulse, (b) Switch1 Stress and (c) Switch2 Stress](image)

IV. COMPARISON

A. Voltage Stress

The voltage stress of the power switches are observed from the simulation results and certain inferences are made. A plot of voltage stress across switches for different duty ratios is shown in the Fig. 22. The voltage stress of the power switch $S_1$ and the diode $D_1$ are both equal to the voltage stress on the power switch in traditional buck boost converter with same input voltage. Similarly, the voltage stress of the power switch $S_2$ and the diode $D_0$ are the same as the voltage stress on the diode in the traditional buck-boost converter. The voltage stresses on the power switches in KY buck-boost converter are very less and same as the input voltage.

![Fig. 22. Comparison about switching stress for different duty ratios](image)

B. Voltage Gain

Voltage Gain of Traditional buck-boost converter is given by

$$M = \frac{V_o}{V_{in}} = \frac{D}{(1-D)}$$

(5)

Voltage Gain of KY buck-boost converter is given by

$$M = \frac{V_o}{V_{in}} = 2D$$

(6)

Voltage Gain of New Transformerless buck-boost converter is given by

$$M = \frac{V_o}{V_{in}} = \frac{D^2}{(1-D)^2}$$

(7)

From the theoretical formulas it is obvious that the New Transformerless buck-boost converter has the better gain among the three. This was further confirmed by the simulation results. The New Transformerless buck-boost converter produced output voltages in wide range without applying extreme duty cycles. Fig. 23 shows the variation in output voltage with change in duty ratios.
C. Complexity And Efficiency

Compared with the traditional buck-boost converter, which has only one power switch, the KY buck-boost converter and New Transformerless, buck-boost converter uses two power switches. Hence the complexity of control is more in the latter two. Traditional buck-boost converter houses minimum number of components compared to the other two. KY buck-boost converter and New Transformerless buck-boost uses two inductors whereas the traditional buck-boost uses only one. KY buck-boost converter has three capacitors, New Transformerless buck-boost has two and traditional buck-boost has only one. Owing to more number of components, the KY buck-boost converter and New Transformerless buck-boost converter are prone to more losses. Hence the efficiency is less for these converters.

The above comparison can be tabulated for easy understanding and is given in Table 2.

Table 2: Comparison between different converters

<table>
<thead>
<tr>
<th>Topology</th>
<th>Traditional buck-boost converter</th>
<th>KY buck-boost converter</th>
<th>New Transformerless buck-boost converter</th>
</tr>
</thead>
<tbody>
<tr>
<td>Switches</td>
<td>1</td>
<td>2</td>
<td>2</td>
</tr>
<tr>
<td>Diodes</td>
<td>1</td>
<td>1</td>
<td>2</td>
</tr>
<tr>
<td>Inductors</td>
<td>1</td>
<td>2</td>
<td>2</td>
</tr>
<tr>
<td>Capacitors</td>
<td>1</td>
<td>3</td>
<td>2</td>
</tr>
<tr>
<td>Voltage Gain (V_out/V_in)</td>
<td>D/(1-D)</td>
<td>D</td>
<td>D/(1-D)</td>
</tr>
<tr>
<td>Voltage Stress of Switches</td>
<td>1/(1-D)</td>
<td>Si</td>
<td>Si/(1-D)</td>
</tr>
<tr>
<td>Voltage Stress of Diodes</td>
<td>1/(1-D)</td>
<td>1</td>
<td>D/(1-D)</td>
</tr>
<tr>
<td>Complexity of small-signal models</td>
<td>Second-order (it has 2 storage elements)</td>
<td>Fifth-order (it has 5 storage elements)</td>
<td>Fourth-order (it has 4 storage elements)</td>
</tr>
</tbody>
</table>

V. EXPERIMENTAL SETUP AND RESULTS

The hardware model of new transformerless buck-boost converter, which is better among the three, is made. In this experiment, the power switches S₁ and S₂ are realized by the power MOSFET IRFP264, the diodes D₁ and D₀ by MUR810, the other circuit parameters are chosen as the same with the MATLAB simulations.

In the step-up mode, for an input voltage of 7V and when a duty ratio of 0.6 is applied an output voltage of 13.8V is obtained. This is shown in the Fig. 26. Here a voltage gain of 1.97 is observed. In the step-down mode, for an input voltage of 4V and when a duty ratio of 0.4 is applied an output voltage of 2.08V is obtained. The output voltage in this case is shown in Fig. 27. High input could not be applied because of the problem of inductor saturation. Also the output voltages in...
both the modes couldn't meet the expectations owing to the losses.

V. CONCLUSION

A new transformerless buck-boost converter, as a fourth-order circuit, realizes the optimization between the topology construction and the voltage gain to overcome the drawbacks of the traditional buck-boost converter and KY buck-boost converter. The main merit of the new transformerless buck-boost converter is that its voltage gain is quadratic of the traditional buck-boost converter so that it can operate in a wide range of output voltages, i.e., this buck-boost converter can achieve high or low voltage gain without extreme duty cycle (0.4-0.6). The simulation results show a power output of 14W for a duty ratio of 0.6. The hardware model of the new transformerless buck-boost converter is made and the simulation results match the hardware results with some error. The hardware model shows a voltage gain of 1.97 in step-up mode for a duty ratio of 0.6. Moreover, the output voltage of this new transformerless buck-boost converter is common ground with the input voltage, and its polarity is positive.

VI. REFERENCE


